## Quiz 7

Chemical Engineering Thermodynamics
February 25, 2021

1) For a throttle valve, such as used in a refrigerator, $\Delta H=0$. You might want to know analytic expressions in terms of $T, P, V, C_{p}, C_{v}, \alpha_{p}$, and $\kappa_{T}$ for the change in entropy and temperature $\left(\mu_{J T}\right)$ across a throttle valve, $\left(\frac{\partial S}{\partial P}\right)_{H},\left(\frac{\partial T}{\partial P}\right)_{H}$. Derive these analytic expressions.
2) Last week we calculated the COP for a 5-ton cascade refrigerator for RNA/DNA using R134a and ethane.
Repeat that calculation of COP using propane and ethane. Determine the values using PREOS.xls. For the reference state use $H_{R}=0 ; T=298 \mathrm{~K} ; P=0.1 \mathrm{MPa} ;$ Real Fluid; and the lowest fugacity root with a solution.

Stage 1 uses propane as a refrigerant and Stage 2 uses ethane. The condenser (8) is at $30^{\circ} \mathrm{C}$, the inter-stage heat exchanger $(6,4)$ is at $-30^{\circ} \mathrm{C}$, and the evaporator (2) is at $-\mathbf{8 6}{ }^{\circ} \mathrm{C}$. The total cooling is $\mathbf{5}$ tons of refrigerant. Assume that the heat exchanger has no thermal loss.
Use PREOS.xls to obtain all values.
The two compressors have an efficiency of $\mathbf{0 . 8 5}$.
1-ton refrigeration $=12,600 \mathrm{~kJ} / \mathrm{h}$
Fill the table values in the process stream table.


Figure 1. Cascade refrigeration cycle. The refrigerants do not mix in the evaporator/condenser. $P-H$ diagrams for the upper and the lower cycles.

ANSWERS: Quiz 7
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$$
\begin{array}{cc}
\left(\frac{\partial S}{\partial P}\right)_{H} & -S U V \\
d H=V d P+T d S & -p G F \\
\left(\frac{\partial H}{\partial P}\right)_{H}^{0}=V\left(\frac{\partial P}{\partial P}\right)_{I F}^{1}+T\left(\frac{\partial S}{\alpha P}\right)_{H} \\
\left(\frac{\partial S}{\partial P}\right)_{H}=\frac{-V}{T}
\end{array}
$$

$$
\left(\frac{\partial T}{\partial P}\right)_{H}
$$

$$
\begin{aligned}
& \text { Trine Pudart Mule }\left(\frac{\partial A}{\partial t}\right)_{P}=C_{p} \\
& \left(\frac{\partial T}{\partial P}\right)_{H}=\frac{-\left(\frac{\partial T}{\partial H}\right)_{p}}{\left(\frac{\partial P}{\partial H}\right)_{T}}=\frac{V\left(T \alpha_{p}-1\right)}{C_{p}} \\
& \left(\frac{\partial H}{\partial P}\right)_{T}=V\left(\frac{\partial P}{\partial P}\right)_{T}+\tau\left(\frac{\partial S}{\partial P}\right)_{T} \\
& =V \bar{T}\left(\frac{\partial V}{\partial T}\right)_{p} \\
& =V T T \alpha_{p}
\end{aligned}
$$

| Stream | P, Mpa | T, ${ }^{\circ} \mathrm{C}$ | $\eta_{\text {e }}$ | State | H, J/mole | S, J/(mole K) | q | $\Delta Q / W_{s,}$ J/mole | m', kg/h | $\underline{Q}$ or $\underline{W}_{s}, \mathrm{~kJ} / \mathrm{h}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ETHANE |  |  |  |  |  |  |  |  |  |  |
| 1 | 0.116 | -86 | - | L/v | -15,300 | -77 | 0.295 | 0 | 183 | 0 |
| 2 | 0.116 | -86 | - | sv | -5,020 | -22 | 1 | 10,300 | 183 | 62830 |
| 3' | 1.06 | 19 | 1 | scv | -904 | -22 | 1 | 4,120 | 183 | 25132 |
| 3 | 1.06 | 32 | 0.85 | SCv | -178 | -19.6 | 1 | 4850 | 183 | 29585 |
| 4 | 1.06 | -30 | - | SL | -15,300 | -80.4 | 0 | -15,100 | 183 | -92110 |
| Propane |  |  |  |  |  |  |  |  |  |  |
| 5 | 0.167 | -30 | - | L/V | -15,500 | -66.3 | 0.36 | 0 | 349 | 0 |
| 6 | 0.167 | -30 | - | Sv | -3,860 | -18.4 | 1 | 11,600 | 349 | 92009 |
| $7{ }^{\prime}$ | 1.08 | 40.6 | 1 | v | 9.32 | -18.4 | 1 | 3,870 | 349 | 30696 |
| 7 | 1.08 | 48.6 | 0.85 | v | 692 | -16.3 | 1 | 4552 | 349 | 36106 |
| 8 | 1.08 | 30 | - | SL | -15,500 | -69.2 | 0 | -16,200 | 349 | -128495 |
| Net COP = | 0.956452905 | Carnot COP = | 1.61 |  |  |  |  |  |  |  |

